June 12, 2019

## STRUCTURAL CALCULATIONS

(Permit Submittal)

## KAHN RESIDENCE ADDITION

18 Brook Bay Road
Mercer Island, WA 98040

Quantum Job Number: 17527.01.01

Prepared for:
DIMARCO ARCHITECTURE
1319 E. Howell St.
Seattle, Washington 98122

Prepared by:
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QUANTUM

## STRUCTURAL DESIGN CRITERIA

KAHN RESIDENCE ADDITION<br>18 BROOK BAY<br>MERCER ISLAND, WA 98105

QUANTUM JOB NUMBER: 17527.01
CODE CRITERIA:
BUILDING CODE 2015 INTERNATIONAL BUILDING CODEBUILDING DEPARTMENTCITY OF MERCER ISLAND
WIND CRITERIA110 MPH; EXPOSURE "C"
. RISK CATEGORY $=1 I$

SEISMIC ZONE ..... SDC = D
SITE CLASS = D
$R=6.5$
$I_{E}=1.0$
$S_{S}=1.46, S_{1}=0.51$
$S_{D S}=0.97, S_{D 1}=0.51$
SNOW ..... 25 PSF
LIVE LOAD (RESIDENTIAL) ..... 40 PSF
SOILS CRITERIA:
ALLOWABLE BEARING PRESSURE (ASSUMED) ..... 1,500 PSF
MINIMUM FOOTING WIDTH CONTINUOUS: 18" MIN., ISOLATED: 24" MIN.
FROST DEPTH ..... 18" MIN
ACTIVE SOIL PRESSURE (RESTRAINED / UNRESTRAINED) ..... 50 PCF / 35 PCF
SEISMIC SURCHARGE PRESSURE (RESTRAINED / UNRESTRAINED) ..... 8H PSF / 6H PSF
PASSIVE SOIL PRESSURE ..... 350 PCF
COEFFICIENT OF FRICTION ..... 0 .35
MATERIALS CRITERIA:
CONCRETE (28 DAY STRENGTH):FOUNDATION/S.O.G - design for 2,500 psi but specify 3,000 for exposure ${ }^{\prime} \mathrm{C}=3,000 \mathrm{PSI}$
REINFORCING STEEL:
GRADE 60 (\#5 BAR OR LARGER) $F Y=60,000 \mathrm{PSI}$
GRADE 40 (\#4 BAR) ..... FY=40,000 PSI
WOOD FRAMING:
2X, 3X, \& 4X FRAMING MBRS ..... HF\#2 OR DF\#2
6X FRAMING MBRS DF\# 1
GLULAM BEAMS ..... 24F-V4 (V8 @ CONT. AND CANT. MBRS)
PARALLAM BEAMSLSL MEMBERS - BEAMS \& HEADERS1.55 E LSL
WOOD SHTG ..... APA RATED

## STRUCTURAL DESIGN CRITERIA

## KAHN RESIDENCE ADDITION

## 18 BROOK BAY

MERCER ISLAND, WA 98105

QUANTUM JOB NUMBER: 17527.01

## ASSEMBLY WEIGHTS

ROOF LOADS

STANDARD ROOFING
1/2" PLYWOOD SHEATHING
ROOF JOISTS @ 24" O.C.
R38 INSULATION
LIGHTS, DUCTS
5/8" GWB
PV ALLOWANCE

MISCELLANEOUS

## COMMENTS

4.0 PSF
1.5 PSF
2.1 PSF
1.0 PSF
0.5 PSF
2.8 PSF
5.0 PSF INCL. W/ MISC.

FOR SEISMIC

|  | 2.5 | PSF |
| ---: | ---: | ---: |
|  | ROOF DL |  |
|  | 17.0 | PSF |
|  |  |  |

FLOOR LOAD

HARDWOOD FLOORING
3/4" SHEATHING
FLOOR JOISTS @ 16" O.C.
LIGHTS, DUCTS
5/8" GWB
MISCELLANEOUS


## QTC Hazards by Location

## Search Information

| Address: | 18 Brook Bay Rd, Mercer Island, WA 98040, USA |
| :--- | :--- |
| Coordinates: | $47.55261290000001,-122.23090780000001$ |
| Elevation: | 93 ft |
| Timestamp: | $2019-06-05 \mathrm{~T} 14: 15: 48.675 Z$ |
| Hazard Type: | Seismic |
| Reference Document: | ASCE7-16 |
| Risk Category: | II |
| Site Class: | D |



Site Class: D

## Basic Parameters

| Name | Value | Description |
| :--- | :--- | :--- |
| $\mathrm{S}_{\mathrm{S}}$ | 1.46 | $\mathrm{MCE}_{\mathrm{R}}$ ground motion (period=0.2s) |
| $\mathrm{S}_{1}$ | 0.506 | $\mathrm{MCE}_{\mathrm{R}}$ ground motion (period=1.0s) |
| $\mathrm{S}_{\mathrm{MS}}$ | 1.46 | Site-modified spectral acceleration value |
| $\mathrm{S}_{\mathrm{M} 1}$ | * null | Site-modified spectral acceleration value |
| $\mathrm{S}_{\mathrm{DS}}$ | 0.973 | Numeric seismic design value at 0.2 s SA |
| $\mathrm{S}_{\mathrm{D} 1}$ | * null | Numeric seismic design value at 1.0 s SA |

* See Section 11.4.8
-Additional Information

| Name | Value | Description |
| :---: | :---: | :---: |
| SDC | * null | Seismic design category |
| $\mathrm{Fa}_{\text {a }}$ | 1 | Site amplification factor at 0.2s |
| Fv | * null | Site amplification factor at 1.0s |
| $\mathrm{CR}_{\text {s }}$ | 0.902 | Coefficient of risk (0.2s) |
| $\mathrm{CR}_{1}$ | 0.898 | Coefficient of risk (1.0s) |
| PGA | 0.625 | MCE ${ }_{\text {G }}$ peak ground acceleration |
| $\mathrm{F}_{\text {PGA }}$ | 1.1 | Site amplification factor at PGA |
| PGA ${ }_{M}$ | 0.688 | Site modified peak ground acceleration |
| $\mathrm{T}_{\mathrm{L}}$ | 6 | Long-period transition period (s) |
| SsRT | 1.46 | Probabilistic risk-targeted ground motion (0.2s) |
| SsUH | 1.619 | Factored uniform-hazard spectral acceleration ( $2 \%$ probability of exceedance in 50 years) |
| SsD | 4.172 | Factored deterministic acceleration value (0.2s) |
| S1RT | 0.506 | Probabilistic risk-targeted ground motion (1.0s) |
| S1UH | 0.564 | Factored uniform-hazard spectral acceleration ( $2 \%$ probability of exceedance in 50 years) |
| S1D | 1.621 | Factored deterministic acceleration value (1.0s) |
| PGAd | 1.398 | Factored deterministic acceleration value (PGA) |

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

## Disclaimer

Hazard loads are provided by the U.S. Geological Survey Seismic Design Web Services.
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Structure: Kahn Residence Addition
Address:
Latitude:
Longitude:

## Structure Classification

Risk Category : II per ASCE Table 1.5-1

Seismic Force-Resisting System: Light-Framed Wood Walls Sheathed with Structural Panels

| $\mathrm{R}:$ | $\mathbf{6 1 / 2}$ | per ASCE Table 12.2-1 |
| ---: | :--- | :--- |
| $\mathrm{W}_{\mathrm{o}}:$ | $\mathbf{2 1 1 2}$ | per ASCE Table 12.2-1 |
| $\mathrm{C}_{\mathrm{d}}:$ | $\mathbf{4}$ | per ASCE Table 12.2-1 |
| $\mathrm{h}_{\mathrm{n}}(\mathrm{ft}):$ | $\mathbf{2 6 . 0 0}$ | height above the base to the highest level of the structure |

## Site Ground Motion

| Reg. Structure 5 Stories or Less: | Yes | Ss $(\max )=1.5$ | Per ASCE 12.8.1.3 |  |
| ---: | :---: | :---: | :---: | :--- |
| $S_{1}(\mathrm{~g}-\mathrm{sec}):$ | 0.51 | $\mathrm{~S}_{\mathrm{S}}(\mathrm{g}-\mathrm{sec}):$ | 1.46 |  |
| Site Class: | D | Per Geotechnical Report | per ASCE Table 20.3-1 |  |
| $\mathrm{S}_{\mathrm{D} 1}(\mathrm{~g}-\mathrm{sec}):$ | $\mathbf{0 . 5 1}$ | $\mathrm{S}_{\mathrm{DS}}(\mathrm{g}-\mathrm{sec}):$ | 0.97 | per ASCE 11.4.4 |

## Fundamental Period per ASCE 12.8.2

| Period Method: <br> Structure Type: | Approximate Fundamental Period <br> All Other Structural Systems |  |
| ---: | :---: | :---: |
| $\mathrm{T}_{\mathrm{L}}(\mathrm{sec}):$ | 6.00 | ASCE Figures 22-12 through 22-16 |
| $\mathrm{Ta}(\mathrm{sec}):$ | 0.23 | $\mathrm{Ct}^{*}$ hnx per ASCE Eq. 12.8-7 |
|  |  |  |
| $\mathrm{T}_{\text {use }}(\mathrm{sec}):$ | 0.23 | $-<=\mathrm{TL}$ |

## Equivalent Lateral Force Procedure Design Base Shear per ASCE 12.8

$$
\begin{array}{rcl}
\mathrm{C}_{\mathrm{s}}: & 0.15 & =\mathrm{S}_{\mathrm{DS}} /\left(\mathrm{R} / I_{E}\right) \text { per ASCE Eq. 12.8-2 } \\
\mathrm{C}_{\mathrm{s} \text { max }}: & 0.34 & =\mathrm{S}_{\mathrm{D} 1} /\left(\mathrm{T}_{\mathrm{a}}{ }^{*} \mathrm{R} / \mathrm{I}_{\mathrm{E}}\right) \text { for } \mathrm{T}<=\mathrm{T}_{\mathrm{L}} \text { per ASCE Eq. 12.8-3 } \\
\mathrm{C}_{\mathrm{s} \text {-max }}: & 9 & =\mathrm{S}_{\mathrm{D} 1}{ }^{*} \mathrm{~T}_{\mathrm{L}} /\left(\mathrm{T}_{\mathrm{a}}{ }^{*}{ }^{*} \mathrm{R} / I_{\mathrm{E}}\right) \text { for } \mathrm{T}>\mathrm{T}_{\mathrm{L}} \text { per ASCE Eq. 12.8-4 } \\
\mathrm{C}_{\mathrm{s} \text {-min }}: & 0.04 & \text { per ASCE Eq. } 12.8-5 \\
\mathrm{C}_{\mathrm{S} \text {-min }}: & -- & =0.5 \mathrm{~S}_{1} /\left(\mathrm{R} / I_{E}\right) \text { for } \mathrm{S}_{1}=>0.6 \mathrm{~g} \text { per ASCE Eq. 12.8-6 } \\
\mathrm{C}_{\mathrm{s} \text {-use }}: & 0.150 & \\
\text { V: } & \mathbf{0 . 1 5 0} \mathbf{W} & =\text { C }_{\text {S-use }}{ }^{*} \mathrm{~W} \text { per ASCE Eq. 12.8-1 }
\end{array}
$$



Structure: Kahn Residence Addition

## Seismic Parameters

| $\mathrm{I}_{\mathrm{E}}:$ | 1.00 | per ASCE Table 1.5-2 |
| ---: | :--- | :--- |
| $\mathrm{S}_{\mathrm{DS}}(\mathrm{g}-\mathrm{sec}):$ | 0.97 | per ASCE 11.4.4 |
| Period $(\mathrm{Sec}):$ | 0.23 | per ASCE 12.8.2.1 |
| $\mathrm{k}:$ | 1.00 | per ASCE 12.8.3 |

## Vertical Distribution of Seismic Forces per ASCE 12.8.3

$$
\begin{aligned}
F_{x} & =C_{v x} V \text { per ASCE Eq. 12.8-11 } \\
C_{v x} & =\left(w_{x} h_{x}{ }^{k}\right) /\left(\text { Sw }_{i} h_{i}^{k}\right) \text { per ASCE Eq. 12.8-12 }
\end{aligned}
$$

| Level | $\mathrm{h}_{\mathrm{x}}(\mathrm{ft})$ | $\mathrm{w}_{\mathrm{x}}(\mathrm{k})$ | $\%$ of $\mathrm{W}_{\text {total }}$ | $\mathrm{w}_{\mathrm{x}}{ }^{*} \mathrm{~h}_{\mathrm{x}}{ }^{\mathrm{k}}$ | $\mathrm{C}_{\mathrm{vx}}(\%)$ | $\mathrm{F}_{\mathrm{x}}(\mathrm{k})$ | $\mathrm{V}_{\mathrm{x}}(\mathrm{k})$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Roof | 26.00 | 2.26 | $64.7 \%$ | 58.79 | $83.1 \%$ | $\mathbf{0 . 4 3}$ |  |
| main | 9.67 | 1.24 | $35.3 \%$ | 11.95 | $16.9 \%$ | $\mathbf{0 . 0 9}$ | $\mathbf{0 . 4 3}$ |
|  |  |  |  |  |  |  | $\mathbf{0 . 5 2}$ |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |

## Vertical Distribution of Seismic Diaphragm Forces per ASCE 12.10.1.1

$$
\begin{aligned}
& \mathrm{F}_{\mathrm{px}}=\left(\mathrm{SF}_{\mathrm{i}} / \mathrm{Sw}_{\mathrm{i}}\right)^{*} \mathrm{w}_{\mathrm{px}} \text { per ASCE Eq 12.10-1 } \\
& F_{p x-m a x}=\left.0.4^{*} S_{D S}{ }^{*}\right|_{E}{ }^{*} W_{p x} \text { per per ASCE 12.10.1.1 } \\
& F_{p x-\text { min }}=0.2{ }^{*} S_{D S}{ }^{*} I_{\mathrm{E}}{ }^{*} \mathrm{~W}_{\mathrm{px}} \text { per per ASCE 12.10.1.1 }
\end{aligned}
$$

| Level | $\mathrm{w}_{\mathrm{px}}(\mathrm{k})$ | $\Sigma \mathrm{w}_{\mathrm{i}}(\mathrm{k})$ | $\mathrm{F}_{\mathrm{x}}(\mathrm{k})$ | $\Sigma \mathrm{F}_{\mathrm{i}}(\mathrm{k})$ | $\mathrm{F}_{\mathrm{px}}(\mathrm{k})$ | Notes |
| ---: | :---: | :---: | :---: | :---: | :---: | :--- |
| Roof | 2.26 | 2.26 | 0.43 | 0.43 | $\mathbf{0 . 4 4}$ | $=\mathrm{Fp}-\mathrm{min}$ |
| main | 1.24 | 3.50 | 0.09 | 0.52 | $\mathbf{0 . 2 4}$ | $=\mathrm{Fp}-\mathrm{min}$ |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |

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Seattle, WA 98101

| Project: | Kahn |
| :---: | :--- |
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| Client: |  |


| Date: $6 / 10 / 19$ | Job No: |  |
| :---: | :---: | :---: |
| Designer: dpf | Sheet: | 2 |
| Checked By: |  |  |

## Wind Loads Criteria

## Wind Load Criteria

Risk Category: II Table 1.5-1 Roof Type: Monoslope Roof

| Basic Wind Speed: | 110 | Figure 26.5 .1 |
| ---: | :---: | :--- |
| Exposure Category: | C | Section 26.7 .3 |

Roof Slope: $\quad 5.5: 12$
Mean Roof HT: $\quad 23.3 \mathrm{ft}$ UP TO 60FT
Wall Ht: 26.0 ft
$\begin{array}{cc}\text { Parapet: } & \text { No } \\ & 26.0 \mathrm{ft} \\ \end{array}$
Wind Topographic Factor, $K_{z t}$ :
per Section 26.8


Terrain Type:
Direction:

Flat Terrain
Upwind of Crest
$\mathrm{L}_{\mathrm{h}}$ : 200 ft dISt UPWIND OF CRESt to half ht of hill or escarp.
H: 200 ft ht. of hill or escarp. reLative to the upwind terrain
x : 50 ft dIST. (UPWIND OR DOWNWIND) FROM THE CREST TO THE BUILDING
h: 23.3 ft mean roof ht above local ground level
$\mathrm{K}_{\mathrm{zt}}$ : 1.00 EQUATION 26.8-1
$\mathrm{K}_{\mathrm{zt}}$ : 1.00 manually input

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## Wind Loads - Main Wind Force Resisting System

ASCE 7-10 Chapter 27 Part 2 - Enclosed Simple Diaphragm, h<160ft

## Wind Load Criteria

Risk Category: II Table 1.5-1
Basic Wind Speed: 110 mph Figure 26.5.1
Exposure Category: C Section 26.7.3
$K_{z t:} \mathbf{1 . 0 0}$ Section 26.8


Note: Roof form may be flat, gable, mansard or hip

FIGURE 27.5-1

## Wall Pressures:

| Transverse | Longitudinal |
| :---: | :---: |
| Wind Direction | Wind Direction |
| $\mathrm{P}_{\mathrm{h}}$ : 28.5 psf | 26.9 psf |
| $\mathrm{P}_{0}$ : 26.9 psf | 25.3 psf |

*Values from ASCE table 27.6-1
*All Values Ultimate (multiply x0.6 for ASD)


FIGURE 27.6-1


## Wind Loads - Main Wind Force Resisting System (Cont.)

ASCE 7-10 Chapter 27 Part 2 - Enclosed Simple Diaphragm, h<160ft

## Roof Pressure:

Slope: 5.5:12
Mean Roof HT: 23.3 ft


Flat Roof
( $\theta<10 \mathrm{deg}$ )

|  | Zone (PSF) |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: |
| Load Case | 1 | 2 | 3 | 4 | 5 |
| 1 | -16.0 | $\mathbf{- 1 7 . 8}$ | $\mathbf{- 2 7 . 4}$ | $\mathbf{- 2 4 . 4}$ | $\mathbf{- 2 0 . 0}$ |
| 2 | 10.8 | $\mathbf{- 8 . 5}$ | $\mathbf{0 . 0}$ | $\mathbf{0 . 0}$ | $\mathbf{0 . 0}$ |


*Values from Table 27.6-2
*All Values Ultimate (multiply x0.6 for ASD)


Hip Roof


Table 27.6-2

## Roof Overhang (PSF)

$$
P_{\text {ovh }}:-20.6 \mathrm{psf}
$$



Figure 27.6-3

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|  | Client: |  | Checked By: |  |  |  |

## Kahn Residence

Wind Base Shear
wind pressure
Sail Area for wind east west
Wind Base shear - east west
28.5 psf

140 sf
3993 pounds

Sail Area for wind north-south
163 psf
Wind Base shear - north south

LIGHT FRAMED WOOD SHEATHED PANEL SHEAR WALL DESIGN
Per IBC 2015, ASCE 7-10, SDPWS 2015 \& NDS 2015
Structure: Kahn Residence Addition
Floor Level: Main

| Sds $=$ | 0.97 |
| ---: | :---: |
| Depth of Floor Framing \& Plates (Clearspan) at Interstory (in) $=$ | 12.00 |


| SW Mark | $L_{s w}(f t)$ | $\mathrm{h}_{\mathrm{SW}}(\mathrm{ft})$ | $\mathrm{h}_{\text {SW }} /$ Lsw | Wall Framing Species | Specific Gravity G | Interstory of Base? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SW GRID South | 12.00 | - | - | - | - | - |
| SW Segment A | 12.00 | 10.83 | 0.90 | DF \#2 | 0.50 | Interstory |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| SW GRID | 0.00 | - | - | - | - | - |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| SW GRID | 0.00 | - | - | - | - | - |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
| SW GRID | 0.00 | - | - | - | - | - |
| SW Segment |  |  | \#DIV/0! | DF \#2 | 0.50 | Base |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |


| SW Mark |  | $\begin{gathered} \hline \text { EQ (lb) Wall } \\ \text { (ULT) } \end{gathered}$ | Wind (lb) Wall (ULT) | Wall DL (Ib) Wall | Wall DL (Ib) End 1 | Wall DL (lb) End 2 | Shear Wall Type | MIN. \# of End Studs | Holdown |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SW GRID | South | 510 | 1997 | - | - | - | - | - | - |
| SW Segment | A | 510 | 1997 |  | 0 |  | SW-6 | 2 | CS16 (1705) |
| SW Segment |  | 0 | 0 |  |  |  | SW-6 |  | No HD |
| SW Segment |  | 0 | 0 |  |  |  | 0 |  | 0 |
| SW Segment |  | 0 | 0 |  |  |  | 0 |  | 0 |
| SW Segment |  | 0 | 0 |  |  |  | 0 |  | 0 |
| SW GRID |  |  |  |  |  |  | - | - | - |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | SW-6 |  | HDU2 (3075DF,2215HF) |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | SW-6 |  | HDU4 (4565DF, 3285HF) |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | SW-6 |  | HDU4 (4565DF, 3285HF) |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | 0 |  | 0 |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | 0 |  | 0 |
| SW GRID |  |  |  |  |  |  | - | - | - |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | SW-6 |  | HDU2 (3075DF,2215HF) |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | SW-6 |  | HDU2 (3075DF,2215HF) |
| SW Segment | 1.20 | \#DIV/0! | \#DIV/0! |  |  |  | SW-6 | 2 | HDU2 (3075DF,2215HF) |
| SW Segment | 1.40 | \#DIV/0! | \#DIV/0! |  |  |  | SW-4 | 2 | HDU5 (5645DF, 4065HF) |
| SW Segment | 1.70 | \#DIV/0! | \#DIV/0! |  |  |  | SW-3 | 2 | HDU8 (6765DF, 4870HF) |
| SW GRID |  |  |  |  |  |  | - | - | - |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | SW-6 |  | HDU2 (3075DF,2215HF) |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | 0 |  | 0 |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | 0 |  | 0 |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | 0 |  | 0 |
| SW Segment |  | \#DIV/0! | \#DIV/0! |  |  |  | 0 |  | 0 |


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| Seattle, WA 98101 | Client: | Checked By: |  |  |  |

## LIGHT FRAMED WOOD SHEATHED PANEL SHEAR WALL DESIGN

Per IBC 2015, ASCE 7-10, SDPWS 2015 \& NDS 2015
Structure: Kahn Residence Addition
Floor Level: Main

| Shear Wall Schedule |  |  |  | $\phi_{D}=0.8$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shear Wall Type | Sheathing Grade, Sheathing Thickness, \& Nail Size | Panel Edge Nail Spacing (in) | Nominal Seismic SW Capacity (plf) | LRFD <br> Seismic SW <br> Capacity (plf) | Sheathing Shear Stiffness, $\mathbf{G}_{\text {a }}$ (lb/in) |
| SW-6 | APA Rated, 15/32", 8d Common | 6 | 520 | 416 | 10 |
| SW-4 | APA Rated, 15/32", 8d Common | 4 | 760 | 608 | 13 |
| SW-3 | APA Rated, 15/32", 8d Common | 3 | 980 | 784 | 15 |
| SW-2 | APA Rated, 15/32", 8d Common | 2 | 1280 | 1024 | 20 |
| 2SW-4 | APA Rated, 15/32", 8d Common | 4 | 1520 | 1216 | 26 |
| 2SW-3 | APA Rated, 15/32", 8d Common | 3 | 1960 | 1568 | 30 |
| 2SW-2 | APA Rated, 15/32", 8d Common | 2 | 2560 | 2048 | 40 |


| SW Segment Mark | Seismic Shear (plf) | Aspect Ratio Reduction | Adjusted Seismic Shear (plf) | Wind Shear (plf) | Adjusted Wind Shear (plf) | Req'd Shear (plf) | Shear Wall Type | Shear Wall Capacity (plf) | Check |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | 43 | 1.00 | 43 | 166 | 119 | 119 | SW-6 | 416 | OK |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-6 | 416 | \#DIV/0! |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-6 | 416 | \#DIV/0! |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-6 | 416 | \#DIV/0! |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-6 | 416 | \#DIV/0! |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-6 | 416 | \#DIV/0! |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-6 | 416 | \#DIV/0! |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-6 | 416 | \#DIV/0! |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-4 | 608 | \#DIV/0! |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-3 | 784 | \#DIV/0! |
|  | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | \#DIV/0! | SW-6 | 416 | \#DIV/0! |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |


| SW Segment Mark | Wall Length Lever Arm (ft) | $\begin{array}{\|c\|} \hline \text { Calculated } \\ \text { Lever Arm (ft) } \\ \hline \end{array}$ | \% Different | Override Wall Length | User Input $\mathrm{M}_{\mathrm{Ot}}$ Lever Arm (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A | 12.00 | 11.79 | 1.77\% | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |
|  |  |  |  | No |  |

Quantum Consulting Engineers LLC 1511 Third Avenue, Suite 323 Seattle, WA 98101

| Project: Kahn | Date: | 6/10/19 | Job No: | 17527.01 |
| :---: | :---: | :---: | :---: | :---: |
|  | Designer: | dpf | Sheet: | 2 |
| Client: 0 | Checked By: |  |  |  |

LIGHT FRAMED WOOD SHEATHED PANEL SHEAR WALL DESIGN
Per IBC 2015, ASCE 7-10, SDPWS 2015 \& NDS 2015
Structure: Kahn Residence Addition
Floor Level: Main

| SW Segment Mark | $\begin{aligned} & \text { Seismic } \\ & \text { Tension (lb) } \end{aligned}$ | ASD Seismic Tension Above (Ib) | Seismic Tension Total (lb) | Wind Tension <br> (Ib) | ASD Wind Tension Above (Ib) | Wind Tension Total (lb) | End 1 Dead <br> (lb) | End 2 Dead <br> (b) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | 322 | 0 | 322 | 1081 | 0 | 1081 | 0 | 0 |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |
|  |  | 0 |  |  | 0 |  |  |  |


| SW Segment Mark | Wind End 1 Eq. 16-15 | $\left.\begin{array}{\|c\|} \hline \text { End } 1 \text { Eq. } 16-16 \\ 16 \end{array} \right\rvert\,$ | $\begin{gathered} \text { End } 2 \text { Eq. } \\ \text { 16-15 } \end{gathered}$ | $\begin{gathered} \text { End } 2 \text { Eq. } 16 \text { - } \\ 16 \end{gathered}$ | Controlling Ten. Load <br> (b) | Holdown | Holdown Capacity (lb) | Status |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | -1081 | -322 | -1081 | -322 | -1081 | CS16 (1705) | -1705 | OK |
|  |  |  |  |  |  | No HD |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | HDU2 (3075DF,2215HF) |  |  |
|  |  |  |  |  |  | HDU4 (4565DF, 3285HF) |  |  |
|  |  |  |  |  |  | HDU4 (4565DF, 3285HF) |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | HDU2 (3075DF,2215HF) |  |  |
|  |  |  |  |  |  | HDU2 (3075DF,2215HF) |  |  |
|  |  |  |  |  |  | HDU2 (3075DF, 2215HF) |  |  |
|  |  |  |  |  |  | HDU5 (5645DF, 4065HF) |  |  |
|  |  |  |  |  |  | HDU8 (6765DF, 4870HF) |  |  |
|  |  |  |  |  |  | HDU2 (3075DF,2215HF) |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |


| Quantum Consulting Engineers LLC | Project: Kahn | Date: | 6/10/19 | Job No: | 17527.01 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1511 Third Avenue, Suite 323 |  | Designer: | dpf | Sheet: | 3 |
| Seattle, WA 98101 | Client: 0 | Checked By: |  |  |  |


| Roof | Results | Current Solution | Comments |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Member Name | Passed | 1 piece(s) $2 \times 12$ Hem-Fir No. 2 @ 24 " OC |  |
| Roof: Joist | Passed | 2 piece(s) $2 \times 4$ Hem-Fir No. 2 |  |
| Roof:Window Header | Results | Current Solution |  |
| Floor | Passed | 1 piece(s) $2 \times 12$ Hem-Fir No. 2 @ 16 " OC |  |
| Member Name | Passed | 1 piece(s) $4 \times 12$ Hem-Fir No. 2 |  |
| Floor: Joist | Passed | 2 piece(s) $2 \times 12$ Hem-Fir No. 2 |  |
| Floor: Support Beam |  |  |  |
| Floor: End Beam |  |  |  |


| ForteWEB Software Operator | Job Notes |  |
| :--- | :--- | ---: |
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Roof, Roof: Joist
1 piece(s) $2 \times 12$ Hem-Fir No. 2 @ 24" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $607 @ 1^{\prime} 13 / 4^{\prime \prime}$ | $2377(3.50 ")$ | Passed (26\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (Adj Spans) |
| Shear (lbs) | $419 @ 11^{\prime} 77 / 1^{\prime \prime}$ | 1941 | Passed (22\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (Adj Spans) |
| Moment (Ft-lbs) | $1403 @ 6^{\prime} 101 / 2^{\prime \prime}$ | 2964 | Passed (47\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (Alt Spans) |
| Live Load Defl. (in) | $0.102 @ 6^{\prime} 101 / 2^{\prime \prime}$ | 0.427 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (Alt Spans) |
| Total Load Defl. (in) | $0.178 @ 6^{\prime} 101 / 2^{\prime \prime}$ | 0.641 | Passed (L/863) | -- | $1.0 \mathrm{D}+1.0$ S (Alt Spans) |

- Deflection criteria: LL (L/360) and TL (L/240).
- Overhang deflection criteria: LL (2L/360) and TL (2L/240).
- Top Edge Bracing (Lu): Top compression edge must be braced at $8^{\prime} 8^{\prime \prime}$ o/c unless detailed otherwise.
- Bottom Edge Bracing (Lu): Bottom compression edge must be braced at $15^{\prime} 4$ " o/c unless detailed otherwise.
- A $15 \%$ increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | ( |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Snow | Total |  |
| 1- Beveled Plate - DF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50 "$ | 261 | 345 | 606 | Blocking |
| 2 - Beveled Plate - DF | $3.50^{\prime \prime}$ | $3.50^{\prime \prime}$ | $1.50^{\prime \prime}$ | 261 | 345 | 606 | Blocking |

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

| Vertical Load | Location (Side) | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $13^{\prime} 9 "$ | $24 "$ | 17.0 | 25.0 | Roof |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

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| :--- | :--- | :--- |
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## Roof, Roof:Window Header

2 piece(s) $2 \times 4$ Hem-Fir No. 2


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $548 @ 0$ | $1823(1.50 ")$ | Passed (30\%) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $414 @ 5^{\prime \prime}$ | 1208 | Passed (34\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Moment (Ft-lbs) | $468 @ 1^{\prime} 81 / 2^{\prime \prime}$ | 748 | Passed (63\%) | 1.15 | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Live Load Defl. (in) | $0.038 @ 11^{\prime} 81 / 2^{\prime \prime}$ | 0.114 | Passed (L/999+) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | $0.071 @ 11^{\prime} 81 / 2^{\prime \prime}$ | 0.171 | Passed (L/581) | -- | $1.0 \mathrm{D}+1.0 \mathrm{~S}$ (All Spans) |

System : Roof
Member Type : Drop Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD Member Pitch : 0/12

- Deflection criteria: LL (L/360) and TL (L/240).
- Top Edge Bracing (Lu): Top compression edge must be braced at 3' $5^{\prime \prime}$ o/c unless detailed otherwise.
- Bottom Edge Bracing (Lu): Bottom compression edge must be braced at $3^{\prime} 5^{\prime \prime} \mathrm{o} / \mathrm{c}$ unless detailed otherwise.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :--- |
|  | Total | Available | Required | Dead | Roof Live | Snow | Total |  |
| 1- Trimmer - HF | $1.50^{\prime \prime}$ | $1.50 "$ | $1.50^{\prime \prime}$ | 253 | 34 | 295 | 582 | None |
| 2 - Trimmer - HF | $1.500^{\prime \prime}$ | $1.50 "$ | $1.50^{\prime \prime}$ | 253 | 34 | 295 | 582 | None |


| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Roof Live <br> (non-snow: 1.25) | Snow <br> (1.15) |
| :--- | :---: | :---: | :---: | :---: | :---: |
| 0 Comments |  |  |  |  |  |

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 and/or tested in accordance with applicable ASTM standards. For current code evaluation reports, Weyerhaeuser product literature and installation details refer to www.weyerhaeuser.com/woodproducts/document-library.
The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
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Floor, Floor: J oist
1 piece(s) $2 \times 12$ Hem-Fir No. 2 @ 16" OC


All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.


- Deflection criteria: LL (L/480) and TL (L/240).
- Top Edge Bracing (Lu): Top compression edge must be braced at 11' 3 " o/c unless detailed otherwise.
- Bottom Edge Bracing (Lu): Bottom compression edge must be braced at $11^{\prime} 5$ " o/c unless detailed otherwise.
- A $15 \%$ increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.
- No composite action between deck and joist was considered in analysis.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Total |  |
| 1 - Hanger on $111 / 4^{\prime \prime} \mathrm{HF}$ beam | 3.50" | Hanger ${ }^{1}$ | 1.50 " | 96 | 320 | 416 | See note ${ }^{1}$ |
| 2 - Hanger on $111 / 4^{\prime \prime} \mathrm{HF}$ beam | 3.50" | Hanger ${ }^{1}$ | 1.50" | 96 | 320 | 416 | See note ${ }^{1}$ |

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.


## Connector: Simpson Strong-Tie

| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 - Face Mount Hanger | Connector not found | N/A | N/A | N/A |  |  |
| 2 - Face Mount Hanger | Connector not found | N/A | N/A | N/A |  |  |


| Vertical Load | Location (Side) | Spacing | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $\mathbf{( 1 . 0 0 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :--- |
| 1 - Uniform (PSF) | 0 to $12^{\prime}$ | $16^{\prime \prime}$ | 12.0 | 40.0 | Residential - Living <br> Areas |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |  |
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## Floor, Floor: Support Beam

## 1 piece(s) $4 \times 12$ Hem-Fir No. 2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :--- | :---: | :---: | :--- | :---: | :--- |
| Member Reaction (lbs) | $2795 @ 2 "$ | $3189(2.25 ")$ | Passed (88\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | $1857 @ 11^{\prime} 23 / 4^{\prime \prime}$ | 3938 | Passed (47\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | $5364 @ 44^{\prime} 61 / 2^{\prime \prime}$ | 5752 | Passed (93\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | $0.076 @ 44^{\prime} 61 / 2^{\prime \prime}$ | 0.219 | Passed (L/999+) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | $0.154 @ 44^{\prime} 61 / 2^{\prime \prime}$ | 0.438 | Passed (L/682) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Top Edge Bracing (Lu): Top compression edge must be braced at $8^{\prime} 11$ " o/c unless detailed otherwise.
- Bottom Edge Bracing (Lu): Bottom compression edge must be braced at 8 ' 11 " o/c unless detailed otherwise.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1- Column - HF | $3.50^{\prime \prime}$ | $2.25^{\prime \prime}$ | $1.97^{\prime \prime}$ | 1454 | 1090 | 783 | 3327 | $11 / 4^{\prime \prime}$ Rim Board |
| 2- Column - HF | $3.50^{\prime \prime}$ | $2.25 "$ | $1.97^{\prime \prime}$ | 1454 | 1090 | 783 | 3327 | $11 / 4^{\prime \prime}$ Rim Board |

- Rim Board is assumed to carry all loads applied directly above it, bypassing the member being designed.

| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> (1.00) | Snow <br> (1.15) | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator


SUSTAINABLE FORESTRY INITIATIVE
Weyerhaeuser

| ForteWEB Software Operator | Job Notes |  |
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## Floor, Floor: End Beam

## $\mathbf{2}$ piece(s) $\mathbf{2 \times 1 2} \mathbf{~ H e m - F i r ~ N o . ~} 2$



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

| Design Results | Actual @ Location | Allowed | Result | LDF | Load: Combination (Pattern) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Member Reaction (lbs) | 1596 @ 3 1/2" | 1823 (1.50") | Passed (88\%) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Shear (lbs) | 1208 @ 1' 2 3/4" | 3375 | Passed (36\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Moment (Ft-lbs) | 4294 @ 6' 3 1/2" | 4482 | Passed (96\%) | 1.00 | $1.0 \mathrm{D}+1.0 \mathrm{~L}$ (All Spans) |
| Live Load Defl. (in) | 0.068 @ 6' 3 1/2" | 0.300 | Passed (L/999+) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |
| Total Load Defl. (in) | 0.268 @ 6' 3 1/2" | 0.600 | Passed (L/537) | -- | $1.0 \mathrm{D}+0.75 \mathrm{~L}+0.75 \mathrm{~S}$ (All Spans) |

System : Floor
Member Type : Flush Beam Building Use : Residential Building Code : IBC 2015 Design Methodology : ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Top Edge Bracing (Lu): Top compression edge must be braced at 4' 10 " o/c unless detailed otherwise.
- Bottom Edge Bracing (Lu): Bottom compression edge must be braced at 12' o/c unless detailed otherwise.
- Applicable calculations are based on NDS.

| Supports | Bearing Length |  |  | Loads to Supports (lbs) |  |  |  | Accessories |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Total | Available | Required | Dead | Floor Live | Snow | Total |  |
| 1 - Hanger on $111 / 4^{\prime \prime}$ HF beam | 3.50" | Hanger ${ }^{1}$ | 1.50 " | 1247 | 252 | 315 | 1814 | See note ${ }^{1}$ |
| 2 - Hanger on $111 / 4^{\prime \prime} \mathrm{HF}$ beam | 3.50" | Hanger ${ }^{1}$ | 1.50" | 1247 | 252 | 315 | 1814 | See note ${ }^{1}$ |

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ${ }^{1}$ See Connector grid below for additional information and/or requirements.


## Connector: Simpson Strong-Tie

| Support | Model | Seat Length | Top Fasteners | Face Fasteners | Member Fasteners | Accessories |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 - Face Mount Hanger | Connector not found | $\mathrm{N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |  | $\mathrm{N} / \mathrm{A}$ |
| 2 - Face Mount Hanger | Connector not found | $\mathrm{N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ |  |


| Vertical Loads | Location (Side) | Tributary Width | Dead <br> $\mathbf{( 0 . 9 0 )}$ | Floor Live <br> $\mathbf{( 1 . 0 0 )}$ | Snow <br> $(\mathbf{1 . 1 5 )}$ | Comments |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| 0 - Self Weight (PLF) | $31 / 2^{\prime \prime}$ to $12^{\prime} 31 / 2^{\prime \prime}$ | $\mathrm{N} / \mathrm{A}$ | 8.6 | -- | -- |  |
| 1 - Uniform (PSF) | 0 to $12^{\prime} 7^{\prime \prime}$ (Front) | $12^{\prime}$ | 12.0 | - | - | wall |
| 2 - Uniform (PSF) | 0 to $12^{\prime} 7^{\prime \prime}$ (Front) | $2^{\prime}$ | 17.0 | - | 25.0 | roof |
| 3 - Uniform (PSF) | 0 to $12^{\prime} 7^{\prime \prime}$ (Front) | $1^{\prime}$ | 12.0 | 40.0 | - | floor |

## Weyerhaeuser Notes

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

| ForteWEB Software Operator | Job Notes |
| :--- | :--- |
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